

Research on Lightweight Material of Frontal Bumper for Midsize Coach

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Abstract: To estimate the aluminum-alloy bumper compared to steel bumper in lightweight and crash safety of midsize coach, a numerical simulation model of coach 100% overlap frontal crash with rigid wall was established by using three dimensional explicit finite element analysis software LS-DYNA 3D, based on China's regulation GB11551-2014 "The protection of the occupants in the event of a frontal collision for passenger car". Three testing parameters were studied, included the reactive force of crash-box, the drive cab integrity and the acceleration of the coach mass center. The results show that: comparing steel bumper, the mass of aluminum-alloy bumper system is decreased 60%, while the system has better absorption crash force curves and crashworthiness of coach body, but the drive cab integrity has become worse.

Key words: coach; bumper; frontal impact; aluminum-alloy material; lightweight

1. Introduction

As the structure of coach frontal energy absorption and the impact force absorption of the outside world, the coach bumper system is a very important component. When collision occurs, it protects the coach body and body accessories. It is important for coach safety, especially flat bus. In view of the demand of the coach in both the crashworthiness and lightweight, the safety performance of the lightweight front bumper system was highly valued. At the same time, with the advance of the lightweight process, the new lightweight material is gradually applied to the body parts, such as aluminum-alloy material, which has the similar mechanical properties, and compared original steel bumper, the mass of aluminum bumper system was reduced by 69%, and the energy absorption of 50%^[1]. In recent years, due to the emphasis on energy saving and environmental protection, the car lightweight has become the important direction of the major automobile enterprises to improve the competitiveness. And the use of aluminum-alloy instead of steel material is one of the major means of reducing the mass of automotive^[2].

In this paper, a new aluminum-alloy bumper system was used to replace the original steel bumper system, and the bumper system was placed on the coach model. Based on the regulations of GB11551-2014^[3], the simulation experiment of coach 100% frontal crash with rigid wall was carried out by comparing the coach model with aluminum-alloy bumper system and steel bumper system along the impact velocity of 30km/h^[4].

2. The establishment of the coach 100% frontal crash model

The coach body is typical half a monocoque body. According to the deformation regularity of coach in collision and in order to save time and ensure the accuracy of the calculation results, it appropriately simplified the coach's body

structure. In order to further ensure the reliability of the calculation results, finite element model was mainly established by shell element properly^[5]. We can simplify the three-dimensional entity model in the CATIA software, and then use the hypermesh/ls-dyna software to establish its finite element model. The related simplification theory of the model can be found in literatures^[6-8].

For coach model, the element size is mainly 10 mm in the main deformation area. In the other area, the element size is mainly 30 mm. The whole coach model is made of 339014 nodes, 339014 square elements, 7521 triangular elements and 136 parts.

Car collision deformation research algorithm mainly used the Lagrangian description increment method^[9]. The related dynamics theory, the control equation and so on in the calculation can be found in literature^[10]. The finite element simulation of coach as follows.

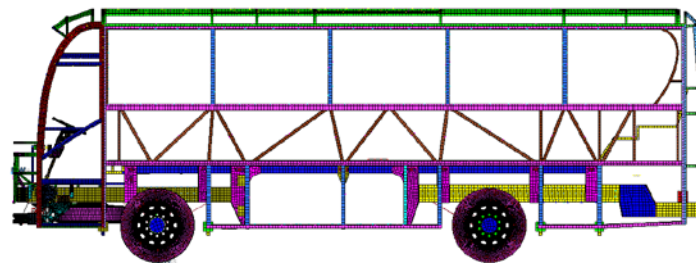


Fig.1 The model of coach 100% frontal crash with rigid wall

3. The selection of coach bumper material

Coach original steel bumper system chosen materials for steel 1 and steel 2, aluminum-alloy bumper system chosen aluminum-alloy1. The material parameters are shown in Table 1. The structure of coach bumper system was shown in Fig.2.

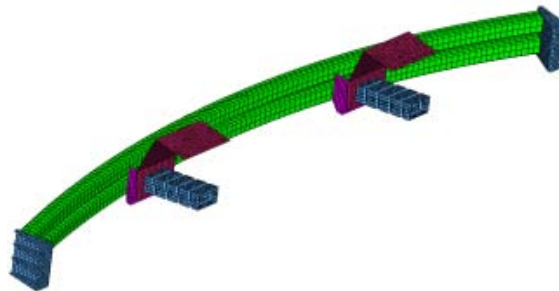


Fig.2 The coach bumper system

Material	σ_s /Mpa	E/Mpa	ν	ρ /(kg/m ³)	C	P
steel 1	245	210000	0.3	7860	40	5
steel 2	570	54000	0.3	7860	40	5
Al-alloy1	308	54000	0.3	2700	40	5

4. The measuring nodes of coach

4.1 The 2 measuring nodes in the left crash-box and the right of crash-box

In coach bumper system, crash-box is an important component to pass force and absorb energy. The reactive force of crash-box can characterize collision energy buffering and impact strength of the bumper system in the process of collision. This coach bumper system consists a left crash-box and a right crash-box, these two crash-boxes have same structure and material. The specific structure of two crash-boxes was shown in the figures below.



Fig.3 The left crash-box and the right crash-box

4.2 The measuring nodes of coach's drive cab

To analyze the influence of Lightweight material substitution on the integrity of the coach drive cab, 12 typical measuring nodes were selected. It contains 6 measuring nodes in the left of coach drive cab and 6 measuring nodes in the right of coach drive cab^[11]. The max displacements variation of 6 measuring nodes along the initial velocity direction in the left of coach drive cab indicates the maximum deformation of the drive cab structure in its left side in the process of coach 100% frontal impact on rigid wall. The max displacements variation of 6 measuring nodes along the initial velocity direction in the right of coach drive cab indicates the maximum deformation of the drive cab structure in its right side in the process of coach frontal impact on rigid wall. The specific positions of those measuring nodes were shown in the figures below:

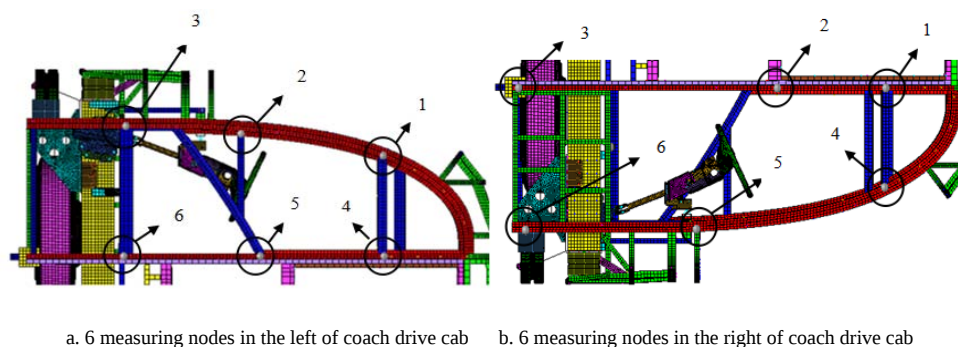


Fig.4 12 measuring nodes in the coach drive cab

4.3 The measuring nodes of coach's mass center

In the process of collision, the value of acceleration along the initial velocity direction in the coach mass center indicates the capacity of energy absorption and crashworthiness of coach structure^[12]. The specific measuring node position of mass center was shown in the Fig.5.

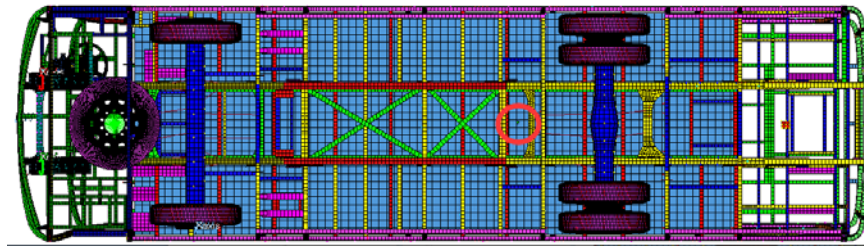
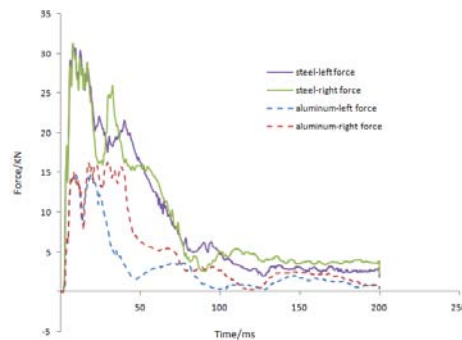


Fig.5 The measuring node position of mass center

5.The results of crash simulation

By the peak value of the curve in the Fig.6, the reactive force of aluminum-alloy bumper system can reach the maximum 16.2KN, and the reactive force of steel bumper system can reach the maximum 31.3KN. In addition, the two kinds reactive force curve of material bumper system can not coincide with the left and right box, which was due to be asymmetric of the structure of coach. It can be seen that the aluminum-alloy bumper system can buffer the impact force in the process of the impact, which can make the structure of body to has better crashworthiness than the steel bumper system.



From the data of 12 measuring nodes in the left and right of coach drive cab in the Table 3 and Table 4, the max displacement variation of 12 measuring nodes of the coach drive cab with aluminum-alloy material bumper system was bigger the steel bumper system. It's shows that aluminum-alloy material bumper system has worse integrity of the coach drive cab than steel bumper system.

Table 3 The max displacement variation of 6 measuring nodes in the left of coach drive cab (Unit: mm)

Bumper classification	1	2	3	4	5	6
Steel material	450.46	223.40	217.24	450.14	241.06	219.65
Al-alloy material	454.80	241.95	226.92	454.73	250.44	229.60
D-value	-4.34	-18.55	-9.68	-4.59	-9.38	-9.95

Table 4 The max displacement variation of 6 measuring nodes in the right of coach drive cab (Unit: mm)

Bumper classification	1	2	3	4	5	6
Steel material	507.37	266.47	240.84	506.58	154.58	129.00
Al-alloy material	508.64	278.10	255.18	507.67	159.35	137.65
D-value	-1.27	-11.63	-14.34	-1.09	-4.77	-8.65

From Fig.7 , the peak value acceleration of coach with steel material bumper system is 24.86g and aluminum-alloy material bumper system is 24.10g , whose impact buffering time increased by about 7ms than steel material bumper system . It shows that the coach structure of the aluminum-alloy bumper system has better energy absorption and crashworthiness than the steel bumper system.

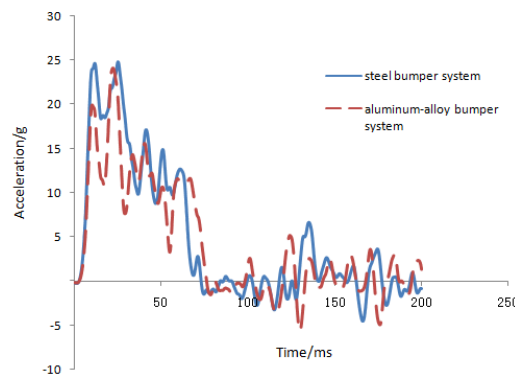


Fig.7 The comparison of acceleration in the coach mass center

6. Discussion and conclusions

1) Compared original steel bumper system, the maximum value of reactive force of aluminum-alloy crash-box was reduced by 15kN, and it can better absorb collision force.

2) Compared original steel bumper system, the max displacement variation of 12 measuring nodes of the coach drive cab with aluminum-alloy material bumper system was bigger, and made the drive cab integrity to be worse.

3) Compared original steel bumper, the peak value acceleration of coach with aluminum-alloy material bumper system was reduced by 4g, and impact buffering time increased by about 7ms. It shows that aluminum-alloy material bumper system made the body of coach to have a better energy absorption and crashworthiness.

4) The mass of aluminum-alloy bumper system was 5.7kg. The mass of steel bumper system was 14-16kg. Compared original steel bumper, the mass of aluminum-alloy was reduced by 60%.

Acknowledgement

This study was sponsored by National Natural Science Foundation of China, grant no.51305374. Fujian Province Outstanding Youth Fund Scientific Research and Talent Cultivation Plan in Universities, grant no.JA14229. Xiamen University of Technology for Foreign Science and Technology Cooperation Foundation, grant no. E201400300.

References

- [1] Cheng Xiusheng, LIU Weihai, HAO Yumin, et al. Optimization of a passenger car's bumper beam for crashworthiness automobile technology [J]. Automotive Engineering, 2011.(10): p.5-9.
- [2] Ding Xiangqun, He Guoqiu, Chen Chengsu, et al. Advance in studies of 6000 aluminum alloy for automobile[J]. Journal of Materials Science & Engineering, 2005.23(2): p.302-305.
- [3] GB11551-2014, The protection of the occupants in the event of a frontal collision for passenger car[S], General Administration of Quality Supervision, Inspection and Quarantine of the People's Republic of China, 2014.
- [4] Tang Youming, Yan Yongpan, Wu Changfeng, et al. Simulation study on front impact safety of medium coach[J]. Bus & Coach Technology and Research, 2012.4: p.47-49.
- [5] Zhong Zhihua, Zhang Weigang, Cao Libo, et al. Automotive crash safety technology[M]. Beijing: China Machine Press, 2003.
- [6] Wu Ping. Research on FEM simulation method of bus body frame rollover impact[D]. Changchun: Jilin University, 2006.
- [7] He Hanqiao, Zhang Weigang. Simulation of safety of high-bed bus under side overturning crash[J]. Mechanical Science and Technology for Aerospace Engineering, 2007.26(7): p.922-925.
- [8] He Hanqiao. The computer simulation of the bus framework safety[D]. Changsha: Hunan university, 2007.
- [9] Kamal M M, Wolf Jr A. Modern automotive structural analysis: 1st Ed [M]. New York: Van Nostrand Reinhold Company, 1982.
- [10] HALLQUIST J O. LS-DYNA theory manual[M]. Livermore: Livermore Software Technology Corporation, 2006.
- [11] Tang Youming, Huang Hongwu, Yi Jiming, et al. Energy absorption study on drive cab of an intercity coach in frontal crash accidents under different velocity [J]. Chinese Journal of Automotive Engineering, 2011. 1(z1): p.114-118.
- [12] Shen Fulin, Deng Jingtao, Xie Xuliang, et al. Research on simulation and improvement of coach frontal crash[J]. China Journal of Highway and Transport, 2010. 23(5): p.113-118.